

The Analysis On Hybrid Superconducting Fault Current Limiter (SFCL) Usage To Limit Short Circuit Fault Current Of 20 Kv Electric Power Distribution In Sengkaling Substation

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ABSTRACT

Keywords

SFCL

Short circuit current

Hybrid SFCL

The occurrence of fault in electrical power system operation is inevitable. The causes of fault in electrical power transmission and distribution system for instances are lightning strikes on transmission canal, tree collapses, or short circuit inter-phases to the ground. In order to protect the equipment and the whole electrical system in Sengkaling Substation and to reduce the short circuit fault current quickly within timeframe of $\frac{1}{2}$ cycle, it requires Superconducting Fault Current Limiter (SFCL) which is going to be placed on the bus that comes close to a critical point. The designing and analysis on the system of before and after hybrid SFCL installment utilize PSCAD software. The simulation result obtained by installing hybrid SFCL in incoming bus 2 (20 kV) was that hybrid SFCL was able to reduce short circuit fault current in $\frac{1}{2}$ initial cycle with L-G fault of 16.77 kA changed to 5.9 kA, L-L-G fault of 35.38 kA changed to 9.15 kA, L-L-L-G fault of 38.36 kA changed to 9.8 kA, and L-L fault of 28.89 kA changed to 4.35 kA. The average percentage of short circuit fault current that was reduced by hybrid SFCL was 74.12%.

1. Introduction

Sengkaling Substation, Malang is a part of distribution system which is located in the area of PT. PLN (State Electrical Company) Malang. Electrical energy usage in Sengkaling Substation tends to be arising every year. This is due to how rapid the development is in Malang and Batu. One of the issues that has occurred in Sengkaling substation is the frequent occurrence of short circuit fault current which happened for ± 18 times throughout 2016. These short circuit fault current happened because of extreme weather which triggered relay trip in feeder supplied by power transformer 4.

With the arising of electrical energy need and bad weather, it demands improvement in operational work of substation and its equipment as the fault increases, the short circuit fault will occur specifically. In order to protect the equipment and the whole electrical system, and to reduce the short circuit fault current quickly within timeframe of $\frac{1}{2}$ cycle, it requires Superconducting Fault Current Limiter (SFCL)[1] which is going to be placed on the bus that comes close to a critical point.

2. The Proposed Method/Algorithm

2.1. Fault in Electrical Power System

Fault in electrical power system is an abnormal state that causes the disruption in electrical power service continuity. Based on its origin, there are two types of fault; fault that is originated from inside the system and one that is originated from outside the system. While based on its nature, fault is divided into two which are temporary and permanent fault. Short circuit fault is caused by phase channel connected to another phase channel or connected to the ground. Short circuit fault may happen in two phases, two phases to the ground, three phases to the ground, and one phase to the ground[3].

2.2. Superconductor Fault Current Limiter (SFCL)

Superconducting Fault Current Limiter (SFCL) is a tool which is able to limit fault current occurs in electrical power network. By applying SFCL, then the occurring fault current is going to be quickly reduced by utilizing the impedance from SFCL[3]. SFCL has an extremely low impedance when it is in a normal state, however when it is in fault state, it has a highly high impedance.

One SFCL is able to limit short circuit fault within less than a half cycle. There are two category of SFCL which are resistive SFCL and saturated ironcore SFCL.

2.3. Resistive Superconducting Fault Current Limiter (SFCL)

Resistive Superconducting Fault Current Limiter (SFCL) is equipped with High Temperature Superconductor (HTS). HTS component is the main component of resistive SFCL. HTS component consists of Superconductor and cooler (Cryostat)[3]. Initially, resistive SFCL only consists of HTS component. Along with the technology development, resistive SFCL has developed into hybrid resistive SFCL with a conventional breaker and hybrid resistive SFCL with fast switch.

2.4. Hybrid Superconducting Fault Current Limiter (SFCL)

Hybrid SFCL is a tool which is able to limit fault current occurs in electrical power network. The outstanding development lies on the part which superconductor does not function as the delimiter for short circuit current but rather only as the sensing for short circuit current and as the switcher for short circuit current to take a turn to Current Limiting Reactor (CLR). Fundamentally, hybrid SFCL consists of three main parts which are fast switch, current delimiter (current limiting part) and high temperature superconductor (HTS)[3]. The structure of hybrid SFCL uses fast switch which is combined with two mechanical switch (vacuum interrupter (VI) and short bar (SB), driving coil and electromagnetic plate (EM) [2].

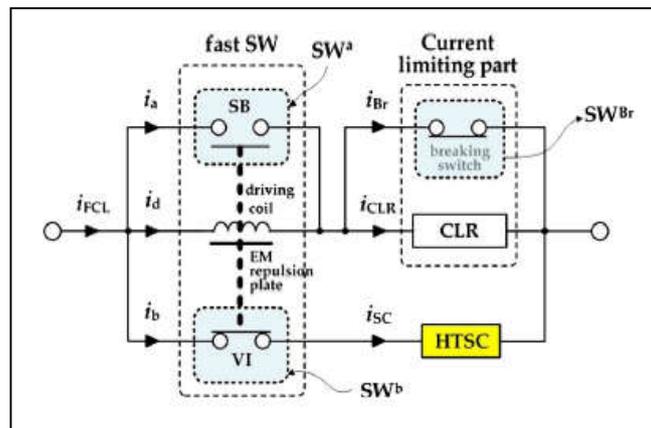


Fig. 1. Hybrid SFCL Configuration Sequence

a. Normal Operational State

In a normal state, superconductor operational temperature was maintained at 77 Kelvin. In this state, HTSC had the impedance of 0 ohm as if it became a conductor with no restriction. Figure 2.2 is a hybrid SFCL sequence in a normal operational state.

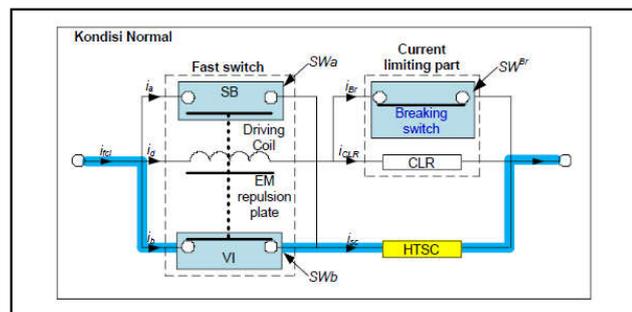


Fig. 2. Normal Operational State

b. Sensing State When Fault Current Occurs

When fault current flows through HTSC and produces heat, it caused HTSC resistance value to increase which triggered fault current to reroute towards drive coil and breaking switch. Figure 2.8 is a hybrid SFCL sequence in sensing state when fault current occurred.

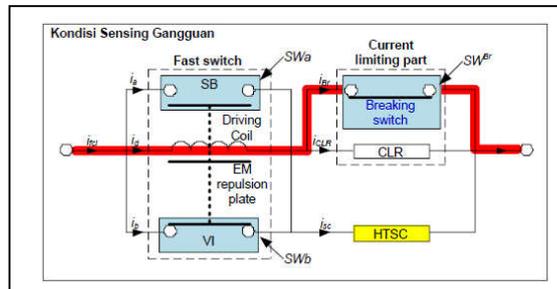


Fig. 3. Sensing State When Fault Current Occurs

c. Fault Occurrence State After Coil is Active

When the current in drive coil hit a certain setting limitation, then magnetic field force produced by the coil would drive SWa, which was initially in a normally open state, to normally close, and would drive SWb, which initially was in a normally close, to normally open. Thus, fault current would flow through SWa and CLR. Fault current that goes through CLR was limited prior to the first 1/2 cycle[5]. Figure 2.9 is a hybrid SFCL sequence in the fault occurrence state after coil was active.

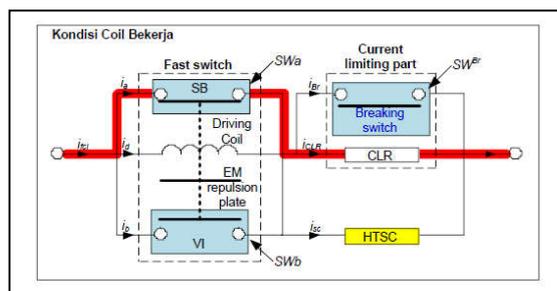


Fig. 4. Fault Occurrence State After Coil was Active

3. Method

3.1. Material and Equipment Used

Materials and equipment used were computer with which it used PSCAD softwares for the testing and calculation.

3.2. Location and Time of Data Collection

Data collection location for this study was technical data belongs to Sengkaling Substation which is one of the substations managed by authorization of PT. PLN P3B for East Java and Bali. The time for data collection was performed in November 1st to November 29th, 2018 as in accordance to requirements set by APP (state company) Malang.

3.3. Data Collection Technique

3.3.1. Direct Observation

By applying this technique, the data needed was specifically the one that relates to general description of observed object which was in regard to what kind of fault occurred in Sengkaling Substation. Thus, this data could be utilized as materials for interview.

3.3.2. Interview

As a start, open interview was performed based on the hands-on observation result data. The next was to perform methodology interview on “The Analysis on Hybrid Superconducting Fault Current Limiter (SFCL) Usage to Limit Short Circuit Fault Current in 150/20 Kv Distribution Network in Sengkaling Substation, Malang” either in separate interviews or focus discussion groups.

3.3.3. Review of Related Literature

Review of related literature was depicted to acquire theories on which it was created as the basis of this study. This study covers the theory comprehension and concept, and suitable method to form framework of thinking in order for this study to be logical and more focused.

3.4. Execution Stages

In order to create the usage simulation on Hybrid Superconducting Fault Current Limiter (SFCL)[6][7] [2] to limit fault short circuit, several stages were performed as below:

1. Entered input data from a single line diagram of Sengkaling Substation which is in a form of transformer data, load data which is in a form of bus data fixed load (P+jQ load), and entered safety data into PSCAD.
2. Performed running simulation on electrical system which was already modeled in PSCAD.
3. Analyzed base case state as the reference for current either in a normal state or fault occurrence state Hybrid Superconducting Fault Current Limiter (SFCL).
4. The next stage was regarding the state which short circuit fault current occurs in a busbar that possessed the highest current. The analysis on short circuit current fault is divided into 4 cases, they are:
 - Short circuit fault of one phase to the ground (L-G)
 - Short circuit fault of phase to phase (L-L)
 - Short circuit fault of two phases to the ground (L-L-G)
 - Short circuit fault of three phases to the ground (L-L-LG)
5. Then, analyzed whether the amount of current that flows through was bigger than the nominal current or not.
6. If it was bigger, then the correct calculation for parameter setting was performed in every Hybrid Superconducting Fault Current Limiter (SFCL) component.
7. The next was performing installation of Hybrid Superconducting Fault Current Limiter (SFCL) to limit short circuit fault current.
8. After short circuit fault current was eliminated, then running simulation was redid by considering the state whether it was still within the limit of current that flows through was bigger than nominal current. If it was still within the limit as it was stated previously, then returned to point 6. If it was not, proceeded to the next point.
9. After that, comparing the result that had been tested among base case states, then the state with short circuit fault current without installation of Hybrid Superconducting Fault Current Limiter (SFCL), and short circuit fault current state with installation of Hybrid Superconducting Fault Current Limiter (SFCL). Setelah itu membandingkan hasil yang telah di uji coba antara kondisi base case, kemudian kondisi dengan arus gangguan hubung singkat tanpa pemasangan Hybrid Superconducting Fault Current Limiter (SFCL) , dan kondisi arus gangguan hubung singkat dengan pemasangan Hybrid Superconducting Fault Current Limiter (SFCL) .
10. Done.

See the below flowchart for more details regarding the Hybrid Superconducting Fault Current Limiter (SFCL) usage to limit short circuit fault current using PSCAD software.

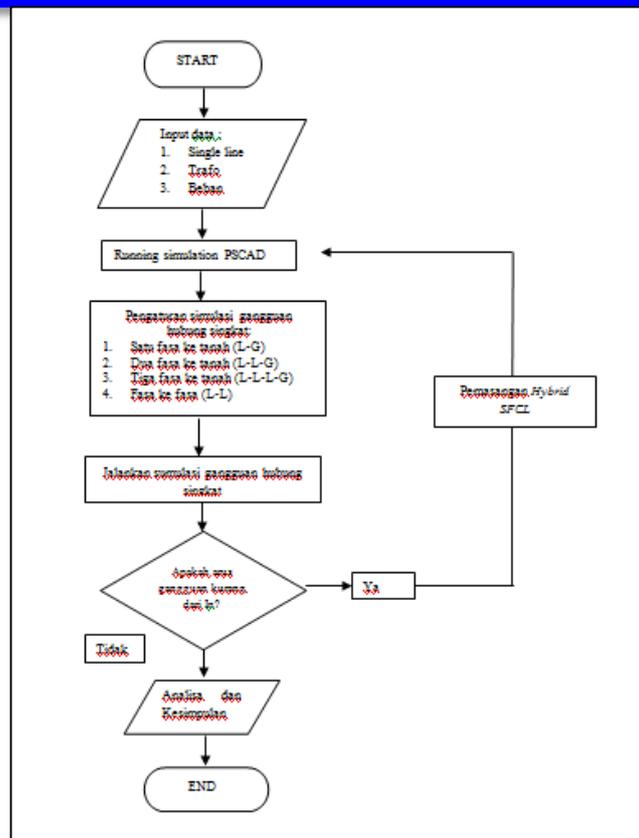


Fig. 5. Problem Solving Flowchart

4. Results and Discussion

4.1. Electrical System Single Line in Sengkaling Substation

Sengkaling Substation owns two distribution transformer; they are Transformer III Unindo 150/20 kV with capacity of 30 MVA/866 A and Transformer IV SHADONG 150/20 kV with capacity of 60 MVA /1732 A. Transformer III serves four feeders which are Junrejo, Pujon, Karangploso and Wastra Indah. Transformer IV serves four feeders which are Seleкта, Batu, Dinoyo, and Tegalgondo. Figure 6 shows a single line diagram of Sengkaling Substation.

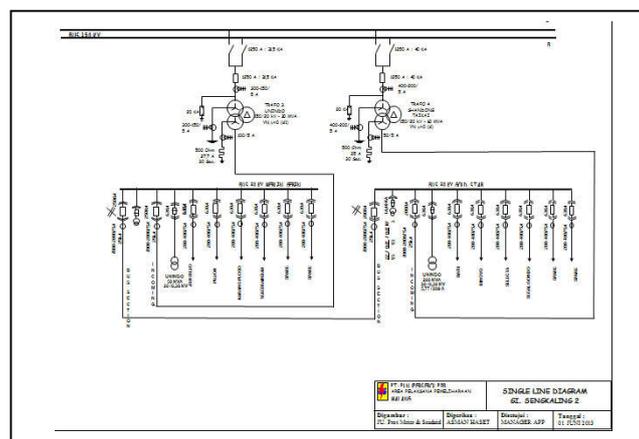


Fig. 6. Single Line Diagram of Sengkaling Substation
 Source: Sengkaling Substation

4.2. Identify the Headings

Power transformer data of Sengkaling Substation was required as transformer model data in PSCAD. Data of transformer III and IV are shown in table 4.1 below:

Table 1. Transformer Data in Sengkaling Substation

	<i>Trafo III</i>	<i>Trafo IV</i>
Brand	UNINDO	SHANDONG
Type	TTUB 150/30000	SFZ11- 60000/150
Power	30 MVA	60 MVA
Impedance	12,5 %	12,43 %
Voltage	150/20 KV	150/20 KV
Grounding Impedance	500 ohm	500 ohm
Winding Circuit	Ynyn0(d1)	Ynyn0(d)

Source: Sengkaling Substation

4.3. Load Data

Load data from Sengkaling Substation was in a form apparent power load data (MVA). Therefore, in order to get active power P and reactive power Q in each feeder, the following equations were used:

$$P = S \times \cos \varphi = V \times I \times \cos \varphi \text{ (MW)} \dots\dots\dots (4.1)$$

$$Q = \sqrt{S^2 - P^2} \text{ (MVAR)} \dots\dots\dots (4.2)$$

Table 2. Maximum Load of Sengkaling Substation

No	Feeder	V (kV)	Cos φ	P (MW)	Q (MVAR)
1	Tegal Gondo	20	0.85	3.247	2.017
2	Selecta	20	0.85	2.635	1.633
3	Dinoyo	20	0.85	2.907	1.801
4	Batu	20	0.85	2.261	1.401
5	Wastra Indah	20	0.85	2.669	1.654
6	Karang Ploso	20	0.85	2.091	1.295
7	Pujon	20	0.85	2.516	1.559
8	Junrejo	20	0.85	1.819	1.127

Source: Sengkaling Substation

4.4. Short Circuit Current Data

MVA value of short circuit in busbar in high voltage 150 kV part, which becomes the supply of Sengkaling Substation, is 2529,44 MVA[10]. Thus, it generated short circuit fault current value as below:

$$I_{sc} = \frac{2529.44 \text{ MVA}}{\sqrt{3} \times 150 \text{ kV}} = 9.736 \text{ kA}$$

4.5. Modeling on Sengkaling Substation

Research data which were in a form of Sengkaling Substation single line diagram data, transformer data, load data, and short circuit data were depicted in PSCAD work sheet. The load in each feeder was modeled in a form of fixed load (P + jQ load). Sengkaling substation single line diagram was further being simulated.

Modeling on Sengkaling Substation single line diagram consisted of three models; they were system prior to fault occurrence, system when fault was set out, and system when fault was set out with SFCL in bus 2 (20 kV).

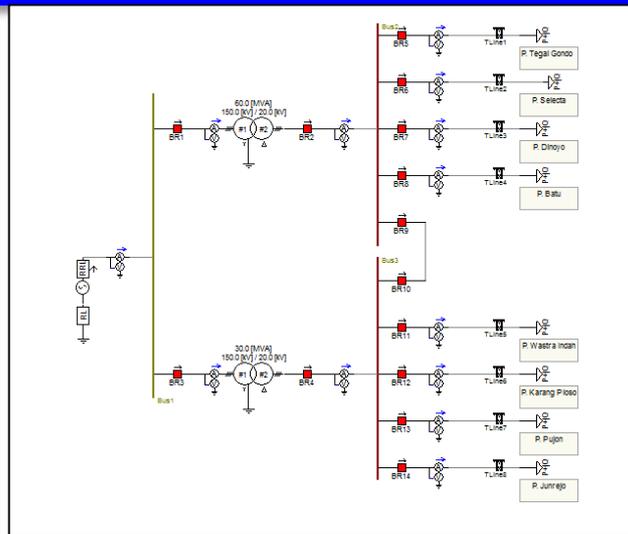


Fig. 7. Modeling on Sengkaling Substation Single Line Diagram prior to Fault Occurrence

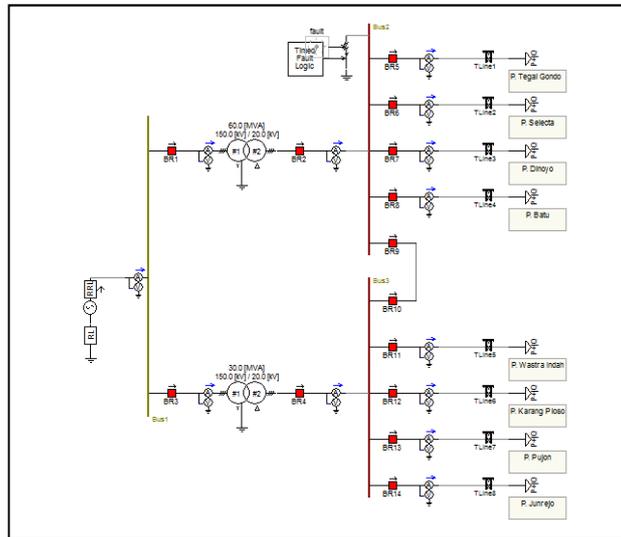


Fig. 8. Modeling on Sengkaling Substation Single Line Diagram When Fault Was Set Out in Bus 2 (20 kV)

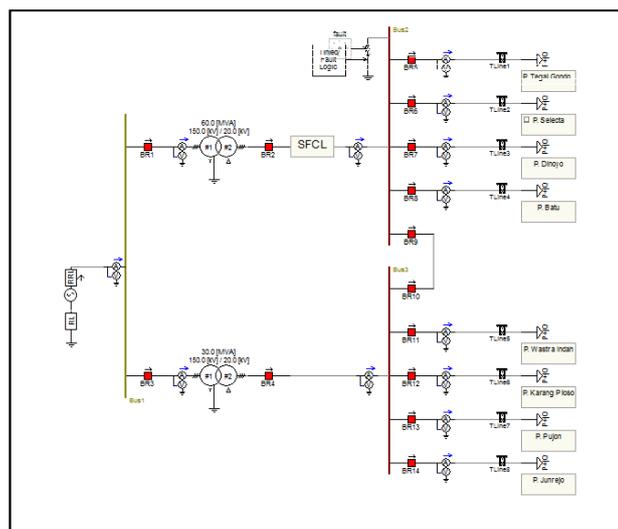


Fig. 9. Modeling on Sengkaling Substation Single Line Diagram When Fault Was Set Out in Bus 2 (20 kV) with Hybrid SFCL

4.6. Modeling on Hybrid SFCL



Fig. 10. Hybrid SFCL Construction

In order to model hybrid SFCL, fast switch was simulated by utilizing breaker (BRKA and BRKC) which functioned as a switch. BRKA was modeled as short bar (SB), BRKC was modeled as vacuum interrupter (VI), and BRKB was modeled as current limiter reactor (CLR).

In a normal state, superconductor operational temperature was maintained at 77 Kelvin. In this state, high temperature superconductor (HTSC) had impedance of 0 ohm. Fault current that flowed through high temperature superconductor (HTSC) and generated heat, it caused high temperature superconductor (HTSC) value increasing which caused fault current to change its course to drive coil and breaking switch. When the current in drive coil hit a certain setting limit, then magnetic field force produced by coil would drive short bar (SB) switch, which was initially open, to close and drive vacuum interrupter (VI) switch, which was initially close, to open. Thus, fault current flowed through short bar (SB) switch and current limiting reactor (CLR). The fault current that flowed through current limiting reactor (CLR) was limited prior to the first 1/2 cycle.

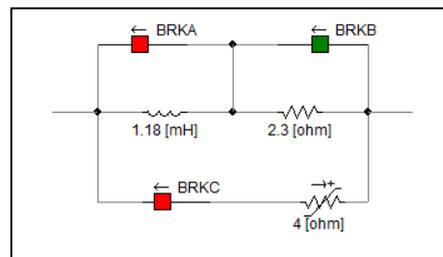


Fig. 11. Modeling for Hybrid SFCL in PSCAD Work Sheet

4.7. Simulation Result

4.7.1. System Prior to Fault Occurrence

The system prior to fault occurrence showed that the form of voltage (kV) waves in bus 1 (150 kV), bus 2 (20 kV), and bus 3 (20 kV).

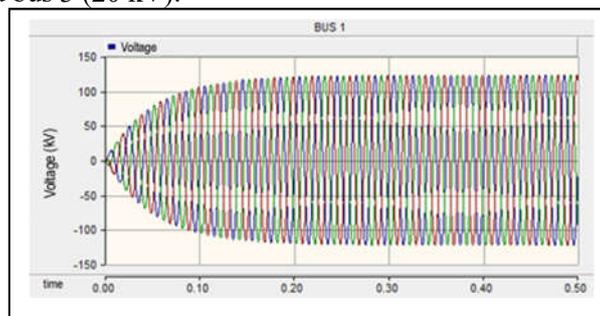


Fig. 12. Voltage Waves in Bus 1 prior to Fault Occurrence

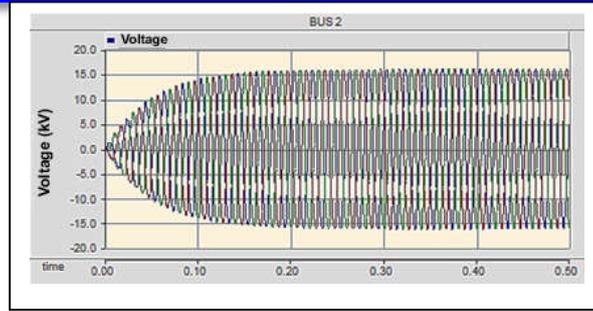


Fig. 13. Voltage Waves in Bus 2 prior to Fault Occurrence

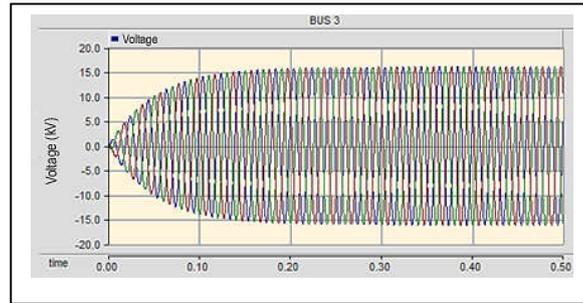


Fig. 14. Voltage Waves in Bus 3 prior to Fault Occurrence

The result of PSCAD simulation running in Figure 12, 13, and 14 showed that the amount of voltage (kV) in bus 1 prior to fault occurrence was $V = 122.31$ kV, voltage (kV) in bus 2 prior to fault occurrence was $V = 16.05$ kV, voltage (kV) in bus 3 prior to vault occurrence was $V = 16.05$ kV.

The form of current waves (kA) in bus 1 (150 kV), bus 2 (20 kV), and bus 3 (20 kV), when the system prior to short circuit fault, were depicted in Figure 15, 16, and 17.

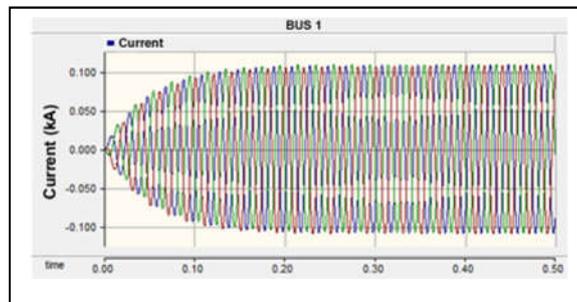


Fig. 15. Current Waves in Bus 1 Prior to Fault

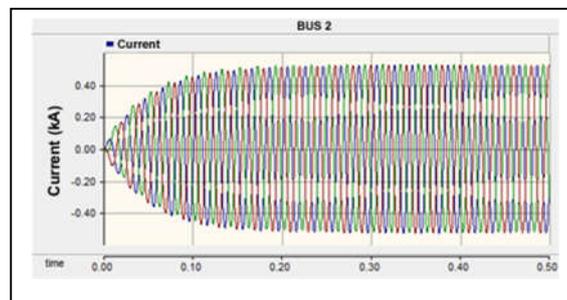


Fig. 16. Current Waves in Bus 2 Prior to Fault

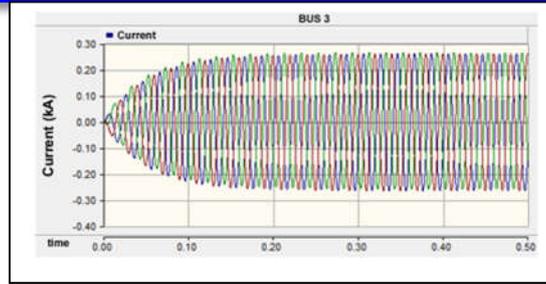


Fig. 17. Current Waves in Bus 3 Prior to Fault

The result of PSCAD simulation running in Figure 15, 16, and 17 showed that the amount of current (kA) in bus 1 prior to fault was $A = 0.1080$ kA, current (kA) in bus 2 prior to fault was $A = 0.5226$ kA, current (kA) in bus 3 prior to fault was $A = 0.2605$ kA.

4.7.2. System When Fault was Set Out in Bus 2 and Hybrid SFCL Installation

The scenario for SFCL placement was based on the highest current value prior to fault. The highest current value occurred in bus 2 (20 kV) was 0.5226 kA. The following figure depicts the time when short circuit fault was set out to current waves form and voltage with and without SFCL.

A. Profiling Results on Current and Voltage before and after Hybrid SFCL Installation When One Phase Fault to the Ground (L-G) Occurred

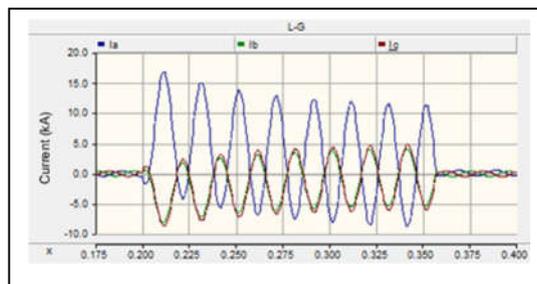


Fig. 18. L-G Short Circuit Fault Current Waves in Bus 2 without Hybrid SFCL

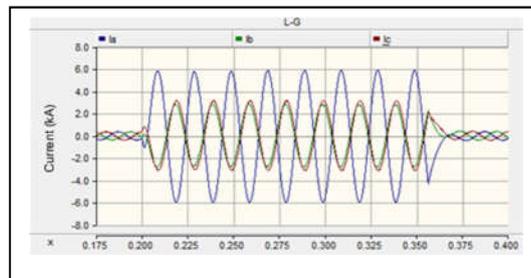


Fig. 19. L-G Short Circuit Fault Current Waves in Bus 2 with Hybrid SFCL

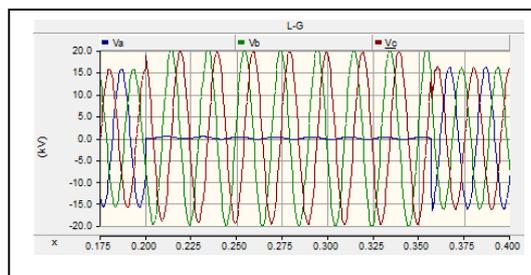


Fig. 20. Voltage Waves When L-G Short Circuit Fault Current Occurred

The above simulation result depicts the amount of current when fault occurred in $t = 0.2$ s with $t = 1.5$ s. By installing hybrid SFCL in the position of incoming bus 2, one phase fault to the ground

experienced reduction on fault current from 16.77 kA to 5.9 kA only within $\frac{1}{2}$ cycle period. It also depicts voltage waves form when it was experiencing reduction on fault up to 100%.

B. Profiling Results on Current and Voltage before and after Hybrid SFCL Installation When Two Phases Fault to the Ground (L-L-G) Occurred

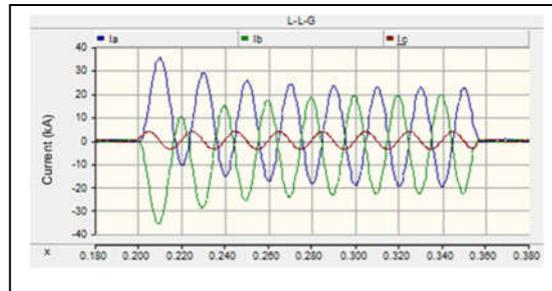


Fig. 21. L-L-G Short Circuit Fault Current Waves in Bus 2 without Hybrid SFCL

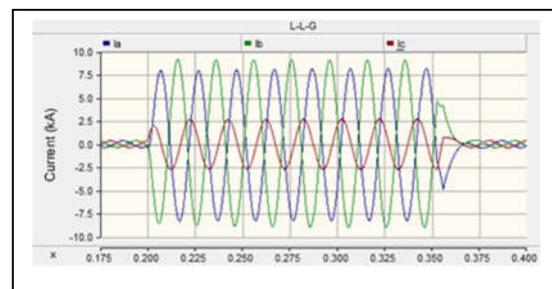


Fig. 22. L-L-G Short Circuit Fault Current Waves in Bus 2 with Hybrid SFCL

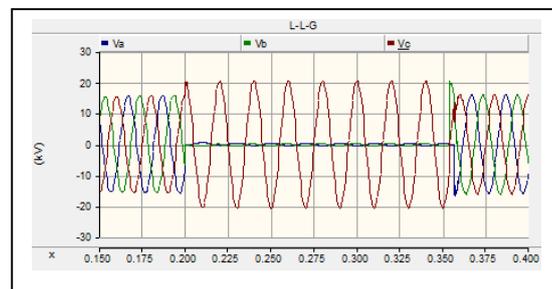


Fig. 23. Voltage Waves When L-L-G Short Circuit Fault Current Occurred

The above simulation result depicts the amount of current when fault occurred in $t = 0.2$ s with $t = 1.5$ s. By installing hybrid SFCL in the position of incoming bus 2, two phases fault to the ground experienced reduction on fault current from 35.38 kA to 9.15 kA only within $\frac{1}{2}$ cycle period. It also depicts voltage waves form when it was experiencing reduction on fault up to 100%.

C. Profiling Results on Current and Voltage before and after Hybrid SFCL Installation When Three Phases Fault to the Ground (L-L-L-G) Occurred

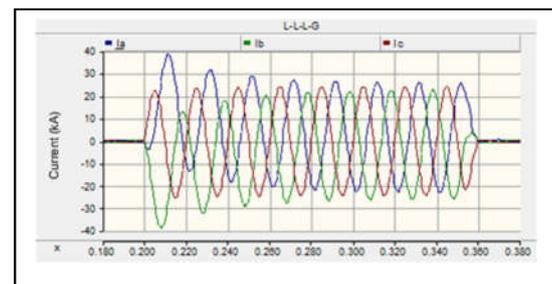


Fig. 24. L-L-L-G Short Circuit Fault Current Waves in Bus 2 without Hybrid SFCL

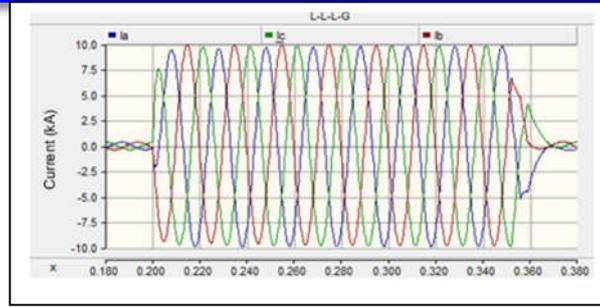


Fig. 25. L-L-L-G Short Circuit Fault Current Waves in Bus 2 with Hybrid SFCL

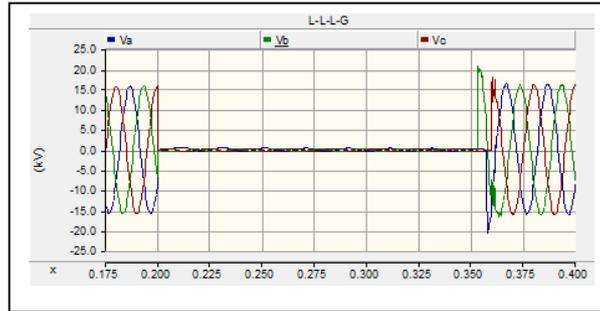


Fig. 26. Voltage Waves When L-L-L-G Short Circuit Fault Current Occurred

The above simulation result depicts the amount of current when fault occurred in $t = 0.2$ s with $t = 1.5$ s. By installing hybrid SFCL in the position of incoming bus 2, three phases fault to the ground experienced reduction on fault current from 38.36 kA to 9.8 kA only within $\frac{1}{2}$ cycle period. It also depicts voltage waves form when it was experiencing reduction on fault up to 100%.

D. Profiling Results on Current and Voltage before and after Hybrid SFCL Installation When Phase to Phase Fault (L-L) Occurred

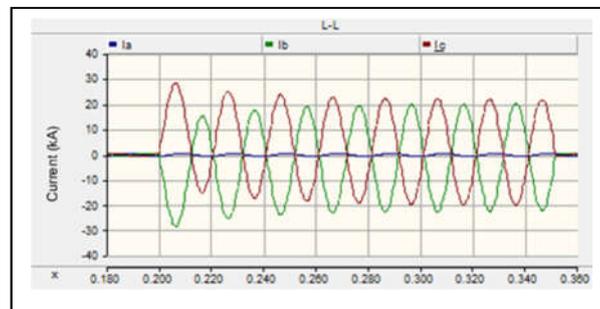


Fig. 27. L-L Short Circuit Fault Current Waves in Bus 2 without Hybrid SFCL

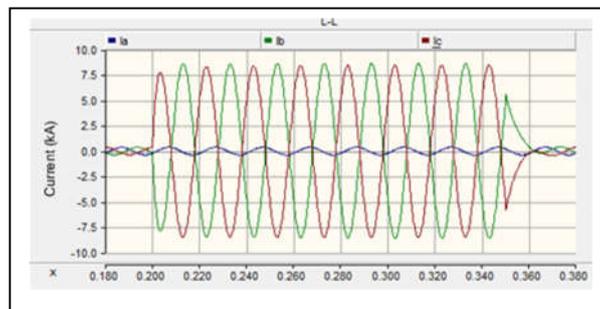


Fig. 28. L-L Short Circuit Fault Current Waves in Bus 2 with Hybrid SFCL

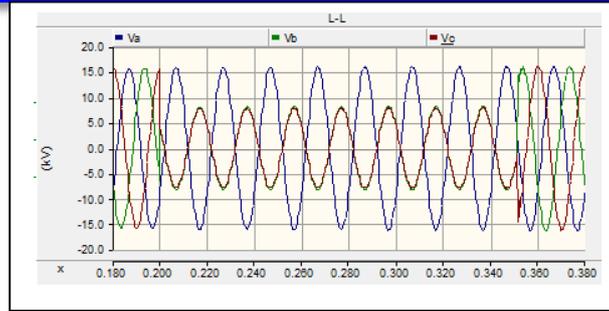


Fig. 29. Voltage Waves When L-L Short Circuit Fault Current Occurred

The above simulation result depicts the amount of current when fault occurred in $t = 0.2$ s with $t = 1.5$ s. By installing hybrid SFCL in the position of incoming bus 2, phase to phase fault to the ground experienced reduction on fault current from 28.09 kA to 4.35 kA only within $\frac{1}{2}$ cycle period. It also depicts voltage waves form when it was experiencing reduction on fault up to 100%.

4.8. Analysis on Simulation Result

Based on the running simulation with all sorts of fault and hybrid SFCL installation, the results are depicted in a table below:

Table 3. Fault Current without and after Hybrid SFCL Installation

	<i>I_{fault}</i> (kA)	<i>I_{SFCL}</i> (kA)	<i>Difference</i> (kA)	<i>Presentage</i> (%)
L-G	16.77	5.9	10.87	64.81
L-L-G	35.38	9.15	25.58	72.3
L-L-L-G	38.36	9.8	28.56	74.45
L-L	28.89	4.35	24.54	84.94

In order to simplify in analyzing simulation results, Table 4.4 can be depicted as the following graphic:

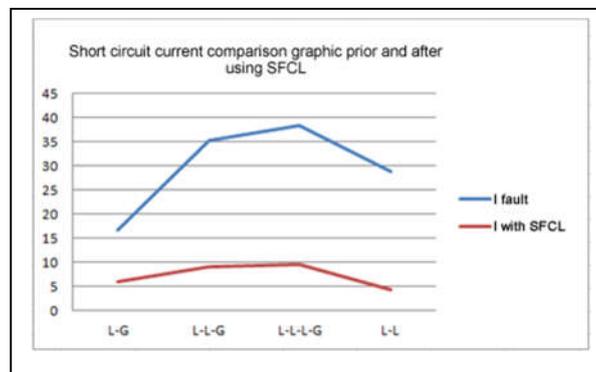


Fig. 30. System Performance Graphic prior to and after SFCL installation

It can be viewed from the graphic that there was a significant reduction occurred in system performance before and after SFCL installation. There were differences in current values before and after SFCL installation. Based on that graphic, red line is lower than blue line with reduction average percentage of 74.12%. Thus, it can be concluded that system performance has been improving after SFCL installation.

5. Conclusion

The conclusions that can be drawn from the effect of hybrid SFCL installation in Sengkaling Substation to reduce short circuit fault current by utilizing PSCAD software are:

1. Hybrid SFCL usage in Sengkaling Substation was able to reduce fault current within the first $\frac{1}{2}$ cycle for L-G fault from 16.77 kA to 5.9 kA. For L-L-G fault, it was from 35.38 kA to 9.15 kA.

For L-L-LG fault, it was from 38.36 kA to 9.8 kA. And for L-L fault, it was from 28.89 kA to 4.35 kA.

2. The percentage of short circuit fault current reduction caused by hybrid SFCL was 74.12%.
3. By installing hybrid SFCL, it could improve system performance in Sengkaling Substation.

References

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